

## Chromium Oxide-Catalyzed Disproportionation of Chlorodifluoromethane: A Mechanism Study

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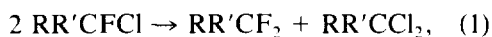
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The facile disproportionation of  $\text{CHF}_2\text{Cl}$  over chrome(III) oxide-based catalysts has allowed the study of catalyst activation and disproportionation as separate processes. Using both a conventional plug-flow microreactor and a TAP reactor, we have found evidence that chrome oxides, in the presence of  $\text{CHF}_2\text{Cl}$ , undergo at least two separate surface transformations before becoming catalytically active toward disproportionation. The first transformation involves a reductive deoxygenation of high-valent surface-Cr species resulting in the formation of  $\text{CO}_2$  and other oxidized products. This reduced surface then reacts with  $\text{CHF}_2\text{Cl}$  to form  $\text{CO}$  and a halogenated, catalytically active surface. It is proposed that catalysis occurs on coordinatively unsaturated halogenated  $\text{Cr}^{3+}$  active sites. An increase in Lewis acidity of the catalyst surface was shown to accompany each transformation step. A brief kinetic study of the disproportionation gave evidence that the reaction does not proceed by a Rideal–Eley mechanism. Examination of initial product distributions, arising from a  $\text{CHF}_3$ -activated catalyst, gave evidence that is consistent with a monomolecular halogen-exchange mechanism. © 1993 Academic Press, Inc.

### INTRODUCTION

The disproportionations of chlorofluorocarbons (CFCs) and hydrochlorofluorocarbons (HCFCs) have been reported to be catalyzed by a variety of metal oxides and halides (1–10):



where R, R' = alkyl, H or halogen. However, the mechanisms of these disproportionations have been ill-defined. Proposed mechanisms may be grouped into three classes. Included are those mechanisms whose principal bond making/breaking processes comprise (a) concerted, bimolecular halogen-exchange reactions between adsorbed organic species (1–3); (b) concerted halogen-exchange reactions between a free organic species and a polarized, complexed species (Rideal–Eley mechanism) (4–6); and (c) concerted, monomolecular exchanges of organic halogen with a metal halide surface (7–10). Class (c) mech-

anisms may be distinguished from the others by the fact that only these mechanisms involve the making and breaking of metal–halide bonds. Proponents of classes (a) and (b) mechanisms have suggested that the active sites of the catalysts are Lewis acid centers capable of strongly polarizing the adsorbed CFC or HCFC prior to reaction. This feature could also be included in class (c) mechanisms, however, Kemnitz *et al.* (9, 10) have suggested that Lewis acid sites are not required by these mechanisms and are unlikely to be necessary. They support this suggestion by their finding that CFCs are only weakly adsorbed on the surfaces of certain metal halides and oxides known to catalyze these reactions.

The empirical finding (11) that catalysts for the disproportionation of the CFCs and HCFCs are usually the same ones found active in isomerizations and halogenations of these compounds suggests that the active sites for *all* of these processes are the same or very similar. To the extent that these

mechanisms are related, studies of the mechanisms of these other processes could yield information quite relevant to disproportionation mechanisms. The elegant work being carried out by Webb, Winfield, and their co-workers (12-15) on the fluorination of CFCs catalyzed by chromia is a case in point. Using isotopic-labeling techniques, these workers have been examining the halogenation reactions of chlorofluoroethanes catalyzed by chromia. By using  $^{18}\text{F}$ - and  $^{36}\text{Cl}$ -labelled hydrogen halides and CFCs, they have shown that halogenation of chlorofluorocarbons occurs at the catalyst surface through a halogen-exchange reaction. Reaction of a chlorofluorocarbon with catalytically active fluorination sites was shown to result in the formation of chlorination sites on the catalyst surface. It was also shown that chromia catalysts contain at least two types of halogenated sites: (1) sites inactive in halogenation of CFCs (suggested to be  $\text{Cr(III)X}_n$ , where  $\text{X} = \text{F}$  or  $\text{Cl}$ ) and (2) sites active towards halogen-exchange with a CFC molecule (suggested to be  $\text{Cr(IV)X}_n$  or  $\text{Cr(VI)X}_n$  where  $\text{X} = \text{F}$  or  $\text{Cl}$ ). Other workers have made similar, though less defined, proposals for CFC fluorination mechanisms. For example, Kolditz *et al.* (5) have offered ESR evidence for the possibility of a redox mechanism involving  $\text{Cr}^{3+}$ ,  $\text{Cr}^{4+}$  and  $\text{Cr}^{6+}$  in CFC fluorinations. Finally, as with disproportionations, it has been proposed (1) that fluorination catalysts must possess Lewis acidity to account for their activity.

There have been few kinetic studies of CFC or HCFC disproportionations. In an early paper Gambaretto (16) reported that the disproportionation of  $\text{CHF}_2\text{Cl}$  over  $\text{AlF}_3$  is first order in reactant. However, no mechanism was proposed to account for this finding. Cavaterra *et al.* (8) reported that the disproportionation of  $\text{CHFCl}_2$  over  $\text{AlF}_3$  followed kinetics consistent with successive reactions of  $\text{CHFCl}_2$  and  $\text{CHF}_2\text{Cl}$  with  $\text{Al-F}$  and  $\text{Al-Cl}$  sites on the catalyst. Adsorption/desorption phenomena were not considered in their model. Kemnitz and Hess (3) studied the kinetics of disproportionation of

$\text{CHF}_2\text{Cl}$  over activated  $\gamma\text{-Al}_2\text{O}_3$  and found the reaction orders to be greater than unity in the organic reactant. This finding was offered as support for a class (a) mechanism. Finally, Okazaki (6) studied the disproportionation of  $\text{CFCl}_3$  over  $\text{FeCl}_3$  on charcoal and found the kinetics obeyed a Rideal-Eley mechanism where the rate-determining step involved the reaction of complexed  $\text{CFCl}_3$  with free  $\text{CFCl}_3$ .

In view of the uncertainties surrounding the mechanisms of these disproportionations, we decided to examine a simple example of such a reaction with the hope of attaining a better understanding of their mechanisms. We chose to examine the disproportionation of  $\text{CHF}_2\text{Cl}$  catalyzed by chromia. Our reasons for choosing this system were threefold. First, this system offers a simple product distribution compared to those found for two-carbon systems. Secondly, this disproportionation was found to be readily achievable at temperatures far below those needed to properly activate the catalyst, thus allowing us to cleanly separate the disproportionation from catalyst-activation processes. Finally, we have felt that an understanding of the mode of behavior of chromia catalysts is of key importance. Since these catalysts have been ubiquitous throughout CFC and HCFC chemistry, we have felt that any understanding of their mode of action in one arena of this chemistry would likely favorably impact the understanding of the others.

#### EXPERIMENTAL

##### *Catalyst Preparation and Characterization*

Two chromia-based catalysts were used in this study. One, designated here simply as  $\text{Cr}_2\text{O}_3$ , is a form of  $\alpha\text{-Cr}_2\text{O}_3$  prepared by the pyrolysis of ammonium dichromate. A sample of this pyrolyzate was pulverized, using a ball mill, to an average particle size of 50 to 75  $\mu\text{m}$ . This material was then washed with warm water and filtered. The resulting solid was dried at 423 K, pressed (at 20,000 psi) into wafers, crushed and

sieved into particles of average size of 250 to 425  $\mu\text{m}$ . The BET surface area of this material, using  $\text{N}_2$ , was found to be 41.4  $\text{m}^2/\text{g}$ . A pore volume, based on nitrogen adsorption, of 0.23  $\text{ml}/\text{g}$  was found. X-ray diffraction (XRD) powder diffractograms showed that the material contained only  $\alpha\text{-Cr}_2\text{O}_3$ . No other crystalline phases could be detected, however, the relatively high surface area suggests the presence of amorphous phases. Transmission electron microscopy revealed a solid consisting of aggregates of platelets consistent with the expected presence of microcrystalline  $\alpha\text{-Cr}_2\text{O}_3$  (17). X-ray photoelectron spectroscopy (XPS), using a VG Scientific spectrometer and  $\text{Mg K}\alpha$  radiation, showed the surface of this material to consist of essentially pure  $\text{Cr}_2\text{O}_3$  (18) containing *ca.* 3 to 4% surface carbon. Analysis for trace metals, using an atomic emission spectroscopic technique, revealed the presence of Ca (275 ppm) and Fe (66 ppm), in addition to Cr. No other metals were found (limits of detection:  $<0.5$  ppm).

The other catalyst, designated here as  $\text{Cr}_2\text{O}_3(\text{C})$  and possessing commercial utility (19), was also prepared from ammonium dichromate pyrolyzate, following the same water wash and drying operations applied to  $\text{Cr}_2\text{O}_3$ . The resulting solid was then compounded with 5.9 wt% of chromium hydroxyacetate [ $\text{Cr}_3(\text{OH})_2(\text{OAc})_7$ ], water and 2 wt% graphite to produce a final catalyst that was pelletized, following a drying step at *ca.* 423 K. This material was then crushed and sieved into particles possessing average sizes of 250 to 425  $\mu\text{m}$ . This final catalyst possessed a surface area of 43.1  $\text{m}^2/\text{g}$  by the BET method, using  $\text{N}_2$ . The nitrogen adsorption-based pore volume was found to be 0.20  $\text{ml}/\text{g}$ . XRD showed this material to be indistinguishable from  $\alpha\text{-Cr}_2\text{O}_3$ . XPS yielded spectra consistent with  $\text{Cr}_2\text{O}_3$  containing *ca.* 7% surface carbon.

A titration technique was used for measuring the presence of high-valent ( $>3^+$ ) chromium on the surfaces of the chrome catalysts being studied. This technique, based on a literature technique (20), con-

sists of titrating (with aqueous  $\text{Na}_2\text{S}_2\text{O}_3$ ) the iodine formed by the reaction of oxidizing surface species with aqueous  $\text{I}^-$ . We improved the convenience of the technique by adding the required amount of HCl near the end of the period that the sample had stood in aqueous KI rather than at its beginning. This modification minimized the need to exclude oxygen from the system. Since the valencies of the high-valent chrome species studied were unknown, the oxidizing capacity of each sample is expressed as Faradays transferred (or equivalently, of  $\mu\text{moles}$  of  $\text{I}^-$  oxidized) per gram of catalyst.

#### *Reactors and Instrumental Analysis Techniques*

Reactions at atmospheric pressures were studied using a 6"  $\times$  4" stainless-steel microreactor heated by an air-stirred silicon carbide bath. Gases were fed to the reactor using calibrated Tylan mass flow controllers. All flows are referenced to standard temperature and pressure conditions of 273 K and 101.3 kPa. Analysis of the reaction products was accomplished using a Hewlett Packard Gas Chromatograph Model 5708A equipped with a 5% Krytox on 60/80 Carbo-pak BHT 20'  $\times$   $\frac{1}{8}$ " column. Catalyst samples (0.5 to 1.0 g) mixed with 600–700  $\mu\text{m}$  silicon carbide (3.5 to 4.0 g), acting as an inert diluent, were used in the reactor. Catalyst activation was carried out by passing a given gas, diluted with  $\text{N}_2$ , over the catalyst at elevated temperatures for a specified time period. Catalyst activities were measured by flowing a 13% mixture of  $\text{CHF}_2\text{Cl}$  in  $\text{N}_2$  over the treated sample at 323 K with a contact time of 0.27 s. Kinetic measurements were carried out on a mixture of 1.0 g of  $\text{Cr}_2\text{O}_3(\text{C})$  and 3.4 g SiC placed in the microreactor. The catalyst was activated by treatment with a stream of 13%  $\text{CHF}_2\text{Cl}$  in  $\text{N}_2$  at 463 K for 16 h. All kinetic measurements were carried out at 296 K in the differential mode with all reactant conversions kept below 9%. The feed flowrates were held constant at 20  $\text{cc}/\text{min}$ . These conditions were chosen to minimize the contribution of

an apparent catalyst poisoning reaction that was significant at higher temperatures. In spite of these precautions, slow catalyst deactivation was still noted and the data was corrected to reflect this using periodic catalyst activity measurements.

Many of our experiments were performed using a TAP (temporal analysis of products) reactor. Since a detailed description of this system is available elsewhere (21), only key features pertinent to this study are given here. The reactor system basically consists of (a) a gas supply system as provided by two high-speed pulse valves and one continuous flow valve, (b) a  $1.25'' \times 0.25''$  reactor containing a packed catalyst bed, and (c) a product gas analysis system as provided by a quadrupole mass spectrometer (UTI 100C). Experimental setup, data acquisition and signal processing were performed on an HP-320 micro computer. The catalyst loadings in this study were generally 0.07 to 0.10 g and were placed in the reactor between two charges of *ca.* 0.20 to 0.30 g each of glass beads of the same particle size. In this study, the quantities of gas passed through the pulse valves were *ca.* 1 to 10 nmol/pulse.

The TAP reactor system offers several advantages over conventional pulsed-reactor systems. Because gases may be pulsed into the reactor at pressures as low as *ca.*  $10^{-7}$  Torr (1 Torr = 133.32 Pa), the contact times of the gases are quite small—of the order of milliseconds. Also, at the low pressures used, gas-gas collisions are considerably reduced. Both of these features offer the possibility of identifying metastable or unstable intermediates not usually observed in a conventional reactor. Another advantage follows from the amount of gas contained in a typical pulse. The pulse valves permit a range of quantities of gas of *ca.* 0.10 to 100 nmol/pulse. This corresponds to the equivalent of *ca.*  $10^{-6}$  to  $10^{-3}$  of monolayer surface coverage of a typical 0.1g catalyst loading possessing a surface area of 50  $m^2/g$ . Thus, under these conditions, the catalyst may be treated either as a constant or slowly diminishing reactant, depending

upon the quantities of gas being fed. In either case, the small quantities of reactants fed permits the surface chemistry of the catalyst to be studied independent of the catalysis. Finally, the low gas pressures and small surface coverages lead to little, if any, surface inhibitions of reactions by most adsorbed gases. This often leads to simplifications in the kinetic expressions used to describe the reactions taking place.

Since the compositions of gases exiting a TAP reactor are analyzed using a mass spectrometer, complications in this analysis often arise due to the overlapping of certain fragmentation patterns from different compounds. Because of this we had to use a matrix algebraic technique employing the relative intensities of several representative *m/e*-values (in this work, *m/e* = 40, 51, 67, 69, and 83) to define the composition of a mixture of  $CHF_2Cl$  and its disproportionation products. Argon (*m/e* = 40) was used as an internal standard (20 mol%). Figure 1 shows typical pulse profiles measured at *m/e* values corresponding to  $CHF_2Cl$  and disproportionation products obtained from pulsing  $CHF_2Cl$  over activated  $Cr_2O_3$  at 473 K. The principal contributors to each *m/e* value are indicated in parentheses.

The TAP reactor was also used to carry out temperature-programmed reaction and desorption studies. In the temperature-programmed reaction mode of operation, a gas was pulsed over a catalyst while the temperature was increased at a constant rate while monitoring a given *m/e* value. For temperature-programmed desorption, we monitored the rate of desorption of gas from a previously-saturated surface as a function of temperature by monitoring a particular *m/e* value characteristic of an adsorbed gas.

Analyses of the reactions of  $CHF_2Cl$  with  $Cr_2O_3(C)$  were also performed on a DuPont 950 Thermal Analyzer. The product gases were analyzed by mass spectroscopy. The sample was first heated in a helium flow (2.0 ml per minute) to 973 K and cooled to room temperature. The TGA-MS experiment was started while flowing 1.5 ml  $CHF_2Cl/min$

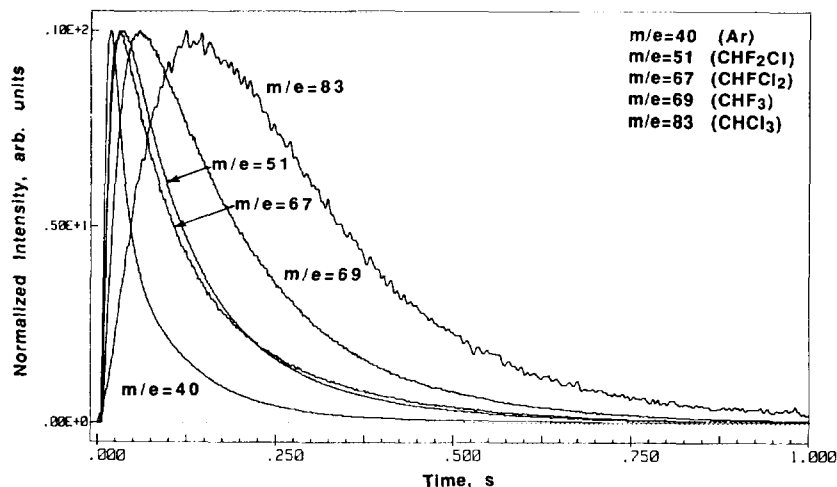


FIG. 1. Pulse profiles of  $\text{CHF}_2\text{Cl}$  and its disproportionation products over  $\text{Cr}_2\text{O}_3$  at 473 K.

and 0.5 ml He/min through the sample region. The temperature of the sample was increased linearly at a rate of 10 K/min. Mass spectra were taken every minute giving a temperature resolution of the product gas analysis of one spectrum per 10 K.

#### Reagents

All reactant gases were obtained from commercial sources and were used as received without further treatment. The gases used were  $\text{N}_2$ ,  $\text{O}_2$ ,  $^{18}\text{O}_2$  (97%),  $^{13}\text{CO}$  (99.4%),  $\text{H}_2$ ,  $\text{HCl}$ ,  $\text{HF}$ ,  $\text{CF}_3\text{Cl}$ ,  $\text{CF}_4$ ,  $\text{CCl}_4$ ,  $\text{CF}_3\text{CF}_3$ ,  $\text{CHF}_3$ ,  $\text{CHF}_2\text{Cl}$ ,  $\text{CHFCl}_2$ ,  $\text{CHCl}_3$ ,  $\text{CH}_3\text{OCH}_3$ , and Ar.

## RESULTS

### Activity Studies

The disproportionation of  $\text{CHF}_2\text{Cl}$  over the chromia catalysts was always accompanied by a further disproportionation of one of the co-products,  $\text{CHFCl}_2$  (3, 22):



These reactions were usually found to proceed cleanly in the presence of the chromia catalysts. At elevated temperatures, equilibrium (at conversions of *ca.* 90 to 95%)

could be approached with less than 1% of byproduct formation. However, the reactions were generally studied at extents of reaction well removed from equilibrium. Both of the  $\text{Cr}_2\text{O}_3$  and  $\text{Cr}_2\text{O}_3(\text{C})$  catalysts displayed similar overall activities suggesting that the same or similar active sites were operating in both catalysts.

Early in our studies it was noted, as others have found (1, 23) for related systems, that the chrome catalysts used here required an activation procedure to realize their catalytic activity. Usually, heating the catalysts to temperatures above *ca.* 448 K for extended periods of time in the presence of  $\text{CHF}_2\text{Cl}$  itself was sufficient to create an active catalyst. However, it was soon found that many other substances served to activate these catalysts. Tables 1 and 2 describe the relative effectiveness of several substances as activators of the  $\text{Cr}_2\text{O}_3$  and  $\text{Cr}_2\text{O}_3(\text{C})$  catalysts toward disproportionation. In these and later tables the activities of the catalysts are measured by their effectiveness in converting  $\text{CHF}_2\text{Cl}$  to  $\text{CHF}_3$ . While, strictly speaking, catalyst activity is directly proportional to percent conversion of  $\text{CHF}_2\text{Cl}$  to  $\text{CHF}_3$  only at the limit of zero percent conversions, we have felt that this

TABLE 1  
Disproportionation Activities of  $\text{Cr}_2\text{O}_3(\text{C})$  Following Treatment<sup>a</sup> with Various Substances

Treatment gas	% Conv. to $\text{CHF}_3$
$\text{N}_2$	<0.01
$\text{CHF}_2\text{Cl}$	39.1
$\text{CHF}_3$	53.2
$\text{CHCl}_3$	1.1
$\text{CCl}_4$	1.7
$\text{CF}_3\text{CF}_3$	29.2
$\text{HCl}$	0.1
$\text{HF}$	0.04

<sup>a</sup>  $\text{Cr}_2\text{O}_3(\text{C})$  (3.7 g) treated with 20% treatment gas in  $\text{N}_2/698 \text{ K}/1 \text{ h}$ .

measure of catalyst activity is an adequate measure for ranking the effects studied here.

Tables 1 and 2 show that all of the effective activators, except for  $\text{HF}$  and  $\text{CF}_3\text{Cl}$ , may also be expected to be the most effective reducing agents. Also, flushing with  $\text{N}_2$  after some treatments was necessary to expose the catalysts activity, presumably due

TABLE 2  
Disproportionation Activities of  $\text{Cr}_2\text{O}_3$  Following Treatment<sup>a</sup> with Various Substances

Treatment gas	% Conv. to $\text{CHF}_3$
$\text{N}_2$	<0.01
$\text{CHF}_3^b$	63.1
$\text{CHCl}_3^c$	23.6
$\text{CF}_3\text{Cl}$	47.6
$\text{CF}_4$	0.5
$\text{CCl}_4^e$	2.2
$\text{HF}^{r,d}$	23.7
$\text{CO}$	46.5
$\text{H}_2$	23.5

<sup>a</sup>  $\text{Cr}_2\text{O}_3$  (0.5 g) treated with 20% treatment gas in  $\text{N}_2/698 \text{ K}/1 \text{ h}$ .

<sup>b</sup> Catalyst wt = 1.0 g.

<sup>c</sup> Catalyst flushed with  $\text{N}_2$  for 1 h at 698 K following treatment.

<sup>d</sup> Induction period (*ca.* 1 h) observed.

<sup>e</sup> Activation temperature = 523 K.

to strong adsorption of activation products. The effectiveness of  $\text{HF}$  as an activator might be linked to the fact that  $\text{HF}$ , as usually supplied, contains small amounts of  $\text{H}_2$ , a demonstrated catalyst activator. We attempted to demonstrate this by flushing the hydrogen out of our  $\text{HF}$  source. However, we were apparently unsuccessful since, even after an overnight purge of our  $\text{HF}$  cylinder, catalytic activity remained significant after treatment with this source of  $\text{HF}$ , albeit with a significant induction period. The reason for the effectiveness of  $\text{CF}_3\text{Cl}$  was not apparent from this test and shall be discussed further under the TAP reactor section. Of particular interest was the finding that a non-halogen-containing compound ( $\text{CO}$  or  $\text{H}_2$ ) could be an effective catalyst activator.

The observation that chromium oxide could be activated using a reducing agent such as  $\text{CO}$ , led us to perform experiments determining the effects of a series of treatments on a single catalyst sample. These treatments consisted of flowing certain gases over a sample of  $\text{Cr}_2\text{O}_3$  for 1 h at a specified temperature. Disproportionation activity was then tested at 323 K following each treatment. Of particular interest was learning whether or not an activated sample could have its catalytic activity quenched and then reactivated. Table 3 summarizes our findings.

The results of Table 3 are strong evidence

TABLE 3  
Successive Disproportionation Activities Following Various Treatments of  $\text{Cr}_2\text{O}_3^a$

Treatment step	Catalyst treatment	% Conv. to $\text{CHF}_3$
1	$\text{N}_2/698 \text{ K}$	0
2	20% $\text{CO}$ in $\text{N}_2/698 \text{ K}$	9.8
3	22% $\text{O}_2$ in $\text{CHF}_2\text{Cl}/\text{N}_2/323 \text{ K}$	8.8
4	20% $\text{O}_2$ in $\text{N}_2/698 \text{ K}$	0
5	20% $\text{CO}$ in $\text{N}_2/698 \text{ K}$	34.1

<sup>a</sup>  $\text{Cr}_2\text{O}_3$  (0.5 g) was treated with each gas at 0.27 s contact time for 1 h.

that an oxidation/reduction cycle is involved in the destruction and creation of active sites for this catalysis. Apparently, the active sites on a chromium oxide catalyst can be created by reduction of surface sites by CO and destroyed by oxidation of these sites with O<sub>2</sub>. However, at 323 K, O<sub>2</sub> does not apparently affect the catalysis significantly. Finally, the catalytic activity could be restored, and even enhanced, by treatment with CO at elevated temperatures following treatment with O<sub>2</sub> at 698 K.

The effect of water on CO-reduced Cr<sub>2</sub>O<sub>3</sub> was examined separately. In this case, a sample of CO-reduced Cr<sub>2</sub>O<sub>3</sub> was treated with a stream of 3% H<sub>2</sub>O in N<sub>2</sub> for ½ h at 698 K. Following this treatment the system was flushed with dry N<sub>2</sub> for an additional 1 h at 698 K in an attempt to drive off any absorbed water. A test of catalytic activity at 323 K showed a 47% reduction in activity, compared to a control sample.

The effects of added gases on the disproportionation of CHF<sub>2</sub>Cl were also of interest in helping to describe the nature of the active sites for this reaction. In a brief study of these effects it was found that when the disproportionation of CHF<sub>2</sub>Cl over Cr<sub>2</sub>O<sub>3</sub>(C) was carried out in the presence of *ca.* 10% dimethyl ether, a Lewis base, the reaction was completely inhibited. When the dimethyl ether was removed from the feed, the catalyst remained inactive. This suggests that the active sites for the disproportionation are Lewis acid sites. A weaker effect was noted with both CO and CO<sub>2</sub>. A mixture of 13% of either CO or CO<sub>2</sub> and 13% CHF<sub>2</sub>Cl in N<sub>2</sub> when passed over an active catalyst at 323 K showed *ca.* 67% or 40%, respectively, of the activity shown in the absence of the added gas. The original catalyst activity was completely restored on replacing the CO by N<sub>2</sub>, however, only *ca.* 70% of the original activity returned on replacement of the CO<sub>2</sub> by N<sub>2</sub>. Finally, HCl, when added to the feed at concentrations of *ca.* 10% at 323 K, completely quenched the catalysis.

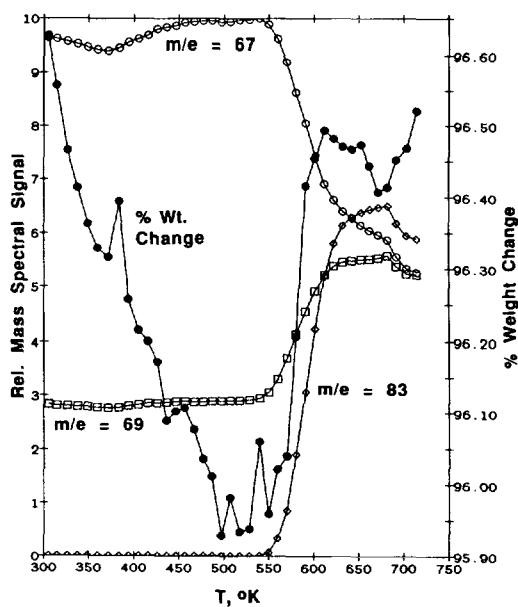


FIG. 2. TGA-MS spectra of products arising from reaction of CHF<sub>2</sub>Cl with Cr<sub>2</sub>O<sub>3</sub>(C).

#### Thermogravimetric Analysis-Mass Spectroscopy (TGA-MS)

In an effort to learn more about the transformations accompanying catalyst activation, the activation of Cr<sub>2</sub>O<sub>3</sub>(C) was followed by TGA-MS, monitoring the weight of the sample as a function of temperature. In addition, the evolution of the gas composition, as a function of temperature while flowing CHF<sub>2</sub>Cl gas, was followed. In Fig. 2 a typical TGA-MS spectrum is shown. Three *m/e* values, each characteristic of each of two of the products and CHF<sub>2</sub>Cl, and the relative change in sample weight are shown as a function of temperature. A sudden increase in weight of the sample at approximately 573 K was observed, which can be ascribed to the uptake of halogen by the chromium oxide. The observed decrease in weight when raising the temperature from 313 K to 573 K is due largely to a baseline drift of the instrument. Accompanying the sample weight increase at *ca.* 573 K, conversion of CHF<sub>2</sub>Cl to the disproportionation products CHF<sub>3</sub> (*m/e* = 69) and CHCl<sub>3</sub> (*m/*

TABLE 4  
XPS Binding Energies (eV) and Atomic% Composition of Treated Samples of Cr<sub>2</sub>O<sub>3</sub><sup>a</sup>

Treatment gas	C 1s	F 1s	O 1s	Cr 2p <sub>3/2</sub>
N <sub>2</sub>	284.6 (3.9)	— (<0.6)	529.8 (58.6)	576.3 (36.0)
HF	284.6 (3.5)	684.2 (10.7)	529.9 (50.6)	576.4 (35.2)
CHF <sub>3</sub>	284.6 (3.4)	684.3 (8.0)	530.2 (52.4)	576.7 (36.3)

<sup>a</sup> Samples were exposed to a flow of 13% treatment gas in N<sub>2</sub>/1 h/698 K. Numbers in parentheses represent atomic % composition. Binding energies are based on C 1s binding energy of 284.6 eV.

$e = 83$ ) was observed, suggesting that an uptake of halogen by the catalyst coincides with the onset of catalytic activity. The decrease in intensity of the  $m/e = 67$  peak can be mainly attributed to the loss of CHF<sub>2</sub>Cl.

#### Surface Analysis

In an effort to understand the effects of the treatment gases on the surface of Cr<sub>2</sub>O<sub>3</sub>, an XPS analysis was carried out on samples which had separately been treated at 698 K with N<sub>2</sub>, CHF<sub>3</sub> and HF. The samples were never exposed to air throughout the procedure. The bonding energies found for Cr and O were consistent with those reported for  $\alpha$ -Cr<sub>2</sub>O<sub>3</sub> (18). No evidence for valence states of Cr other than 3<sup>+</sup> could be found in any of the samples. The binding energies found for fluorine were consistent with those previously found for surface chromium fluorides (2). The O:Cr ratio decreased as the extent of surface fluorination increased. Thus, the surfaces of both the CHF<sub>3</sub>- and HF-treated Cr<sub>2</sub>O<sub>3</sub> samples apparently contained significant amounts of chromium fluorides. Table 4 summarizes our findings.

Similar results were obtained from Cr<sub>2</sub>O<sub>3</sub>(C). Surface area measurements carried out on the treated samples of Cr<sub>2</sub>O<sub>3</sub>(C) showed the surface areas of the HF- and CHF<sub>3</sub>-treated samples to have changed by less than 10% from that measured (43.1 m<sup>2</sup>/g) for the N<sub>2</sub>-treated sample.

#### Microreactor Kinetics

The kinetic behavior of the disproportionation was briefly investigated using

Cr<sub>2</sub>O<sub>3</sub>(C) in an effort to distinguish between various possible mechanisms. Table 5 summarizes our findings.

We examined the fit of only one kinetic model derived from a class (b) mechanism, described in the introduction. In this model, the rate-determining step was defined as the reaction of free CHF<sub>2</sub>Cl with surface-bound CHF<sub>2</sub>Cl. This model did not give a satisfactory fit to the data. Class (a) mechanisms were not examined since the independent information, *vide infra*, indicated that these mechanisms were not operative. Kinetic models corresponding to a class (c) mechanism, where the rate-determining steps involved either carbon-halogen bond breaking/making or product desorption, were constructed but not tested. These models involved reaction, adsorption and desorption processes of each of the four HCFCs with two postulated halogenated metal sites. These sites were distinguished by the nature of the exchangeable halogen bonded to each site. The resulting models consisted of 14 separate processes. A portion of one of the models, involving the processes associated with CHF<sub>2</sub>Cl is shown in Scheme 1.

- (1) CHF<sub>2</sub>Cl + S-F = CHF<sub>2</sub>Cl\*S-F
- (2) CHF<sub>2</sub>Cl\*S-F = CHF<sub>3</sub>\*S-Cl
- (3) CHF<sub>3</sub>\*S-Cl = CHF<sub>3</sub> + S-Cl
- (4) CHF<sub>2</sub>Cl + S-Cl = CHF<sub>2</sub>Cl\*S-Cl
- (5) CHF<sub>2</sub>Cl\*S-Cl = CHFCl<sub>2</sub>\*S-F
- (6) CHFCl<sub>2</sub>\*S-F = CHFCl<sub>2</sub> + S-F

S-Cl and S-F represent halogenated catalyst sites

SCHEME 1. Halogenated-Site Mechanism



TABLE 5

Product Partial Pressures from Disproportionation of CHF<sub>2</sub>Cl

CHF <sub>2</sub> Cl <sup>b</sup>	CHF <sub>3</sub> <sup>a</sup>	CHFCI <sub>2</sub> <sup>a</sup>	CHCl <sub>3</sub> <sup>a</sup>
0.716	0.480	0.034	0.237
0.717	0.516	0.045	0.258
1.83	0.840	0.092	0.388
1.90	0.796	0.073	0.365
3.30	1.04	0.109	0.460
3.40	1.04	0.134	0.463
6.64	1.31	0.180	0.637
6.67	1.53	0.234	0.666
9.85	1.70	0.243	0.751
10.0	1.62	0.275	0.700
10.1	1.60	0.244	0.760
10.2	1.65	0.316	0.766
20.2	2.01	0.374	1.03
20.6	2.42	0.434	0.912
44.3	3.07	0.589	1.12

<sup>a</sup> Partial pressures = atm × 10<sup>3</sup> (1 atm = 101.3 kPa).<sup>b</sup> Partial pressures = atm × 10<sup>2</sup>.

This model yielded an expression for the rate of formation of CHF<sub>3</sub> that contained fourteen adjustable parameters. After combining certain parameters, while still retaining the sense of the model, and requiring that the net halogen content of the catalyst remain constant, an expression with nine parameters was finally obtained. With such a large number of adjustable parameters remaining, any attempt to fit this model to the limited data available was considered imprudent. As a result, it was possible to eliminate only the Rideal-Eley mechanism (class (b) mechanism) described in the introduction.

Attempts to measure activation energies of the disproportionation failed, presumably due to the formation of an unknown substance (HCl?) which slowly poisoned the catalysis at elevated temperatures. However, at temperatures above *ca.* 448–473 K the reaction rates sharply accelerated, possibly due to the desorption of this poison from the catalyst surface.

#### TAP Reactor Studies

(a) *Catalyst activation.* The reactions of CHF<sub>3</sub> and CHF<sub>2</sub>Cl with Cr<sub>2</sub>O<sub>3</sub> were first ex-

amined in an attempt to identify the gaseous products formed during the catalyst activation process noted earlier. Pulsing either of these gases over Cr<sub>2</sub>O<sub>3</sub> at temperatures between 523 and 798 K resulted in significant reaction. For example, pulsing CHF<sub>3</sub> over Cr<sub>2</sub>O<sub>3</sub> at temperatures between 698 and 798 K yielded increased pulse intensities for certain *m/e* values indicating the formation of H<sub>2</sub>O, HF and CO<sub>2</sub>. CO was also observed, however, this could not be distinguishable from a signal resulting from backscattering processes occurring at the ion-pump. The formation of COF<sub>2</sub> could not be ruled out since COF<sub>2</sub> possesses *m/e* values coinciding with CHF<sub>3</sub>. However, only very small amounts of COF<sub>2</sub> could have been present since the pulse shapes at the relevant *m/e* values were essentially identical to those previously measured for CHF<sub>3</sub>. The formation of oxygenated products implies the concurrent formation of surface metal fluorides, as was confirmed previously by our XPS studies. Similar results were obtained with the more reactive CHF<sub>2</sub>Cl indicating surface halogenation and formation of oxygenated gaseous species occurred here as well.

The formation of CO<sub>2</sub> upon pulsing CHF<sub>3</sub> over Cr<sub>2</sub>O<sub>3</sub> suggested that our Cr<sub>2</sub>O<sub>3</sub> sample contained oxidizing sites (Cr<sup>4+</sup> or Cr<sup>6+</sup> ?) that were reduced by the CHF<sub>3</sub>. To test this we pulsed CO over Cr<sub>2</sub>O<sub>3</sub> at elevated temperatures and found that indeed CO<sub>2</sub> was readily formed, indicating the reduction of surface sites. Figure 3 shows a comparison between the CO<sub>2</sub> formed (based on *m/e* = 44) from CHF<sub>3</sub> pulsing and from CO pulsing at 798 K. The amount of CO<sub>2</sub> formed from CO treatment (15.1 μmoles/g) was approximately three times that formed from CHF<sub>3</sub> (4.6 μmoles/g). This may have occurred, in part, because of differences in the thermal stabilities of the samples (24). Support for this possibility came when we observed *more* CO<sub>2</sub> formed from CHF<sub>3</sub> at 698 K (12.1 μmoles/g) than at 798 K (4.6 μmoles/g), suggesting that thermal depletion of the oxidation potential was less significant at lower temperatures.

Chromium oxides, prepared by the pyrol-

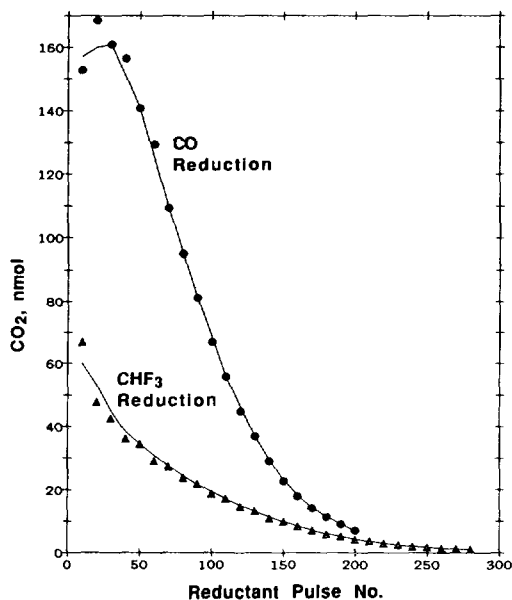


FIG. 3. Carbon dioxide formation from reductions of  $\text{Cr}_2\text{O}_3$  by  $\text{CHF}_3$  and  $\text{CO}$  at 798 K.

ysis of ammonium dichromate, are well known to contain significant amounts of high-valent surface Cr species (20, 25). Most of these species consist of water-soluble  $\text{Cr}^{6+}$  compounds, extractable by simple water washing. Since our catalysts had been thoroughly washed during their preparation, any high-valent chrome species remaining were not water soluble. This suggested that the high-valent chrome species remaining on  $\text{Cr}_2\text{O}_3$  were not separate  $\text{Cr}^{6+}$  oxide phases but may have consisted of mixed  $\text{Cr}^{m+}/\text{Cr}^{n+}$  ( $n, m = 3, 4, 5, \text{ or } 6$ ) or pure  $\text{Cr}^{4+}$  or  $\text{Cr}^{5+}$  oxide phases which are less likely to be water soluble. As a further test for the presence of high-valent Cr species on  $\text{Cr}_2\text{O}_3$  we found, on applying the iodometric titration test, that a sample of  $\text{Cr}_2\text{O}_3$  yielded an oxidation capacity of  $6.2 \times 10^{-5}$  Faradays/g. This compares to a value of  $3.0 \times 10^{-5}$  Faradays/g obtained from the  $\text{CO}$ -oxidation technique. The lower value obtained using the  $\text{CO}$ -reduction technique may have been due to a loss of oxidation capacity resulting from the thermal treatment of the sample

(24). This was checked by measuring the oxidation capacity of a sample that had been exposed to  $\text{N}_2$  for 1 h at 698 K and found to give an oxidation capacity, using the iodometric technique, that was 15% of an unheated sample. Based on these values and the reported surface area ascribed to a monolayer of 1 g of  $\text{Cr}_2\text{O}_3$  (26), we estimate that the percentage of surface Cr atoms that are in valence states greater than  $3^+$  ranges from 1.4 to 8.4%, depending upon the analysis technique used and the valence states of the Cr. Finally, testing of the aqueous phase of a water-washed sample of  $\text{Cr}_2\text{O}_3$  by the iodometric test showed the absence of any high-valent Cr, verifying the absence of water-extractable chromates for this material. As expected, testing of this water-washed  $\text{Cr}_2\text{O}_3$  as a disproportionation catalyst showed no decline in activity compared to an unwashed sample.

As noted above, our microreactor studies showed that the catalysis could be quenched by treatment with oxygen at 698 K. In order to study the reaction of oxygen with the catalyst in more detail, we investigated the oxidation of active catalysts with  $\text{O}_2$  in the TAP reactor. A sample of  $\text{Cr}_2\text{O}_3$ , previously reduced with  $\text{CO}$  at 698 K, was pulsed with  $\text{O}_2$  and an uptake of  $\text{O}_2$  was observed. The oxidized catalyst was again reduced with  $\text{CO}$  and, finally, again oxidized with  $\text{O}_2$ . The progress of these redox reactions was followed by measuring the maximum signal intensity of each pulse of gas (at  $m/e = 44$  and 32) as a function of pulse number. Figure 4 shows the results of this experiment. The reproducibility of the cycle shows the complete reversibility of both the reduction and oxidation processes at 698 K. The relative stability of the system was also demonstrated by the observation that the extent of  $\text{CO}$  uptake by the  $\text{Cr}_2\text{O}_3$  was unchanged after standing for 10 min at 698 K. In a similar study, involving the oxidation of  $\text{CO}$ -reduced  $\text{Cr}_2\text{O}_3$  with  $^{18}\text{O}_2$ , it was noted that when the catalyst was allowed to stand for eight minutes at 798 K, a sharp increase in oxygen uptake occurred. This phenomenon

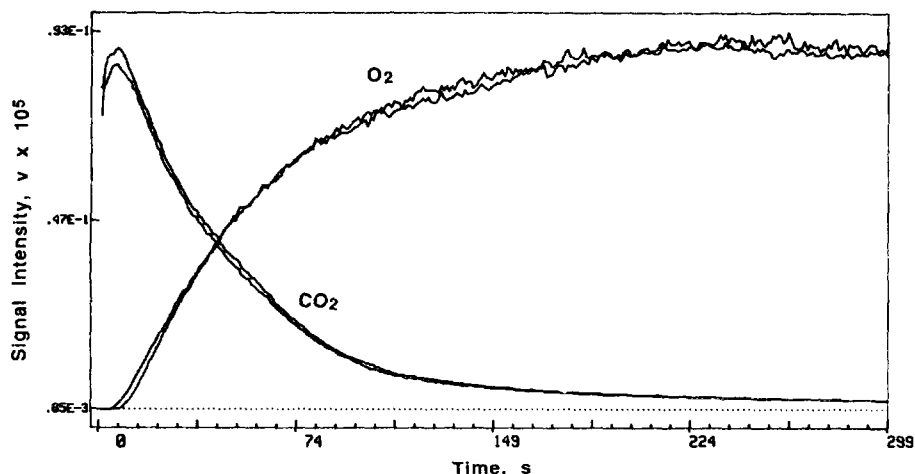


FIG. 4. Redox reactions of  $\text{Cr}_2\text{O}_3$  as function of pulse number at 698 K.

suggests that the surface oxygen atoms, at this higher temperature, are either highly mobile and diffuse away from the active sites leaving vacancies behind or that they desorb relatively easily.

As noted earlier in our microreactor studies, treatment of  $\text{Cr}_2\text{O}_3$  with  $\text{CF}_3\text{Cl}$  at 698 K/1 h was sufficient activation for F-22 disproportionation to occur. This result was unexpected since it was hard to see how  $\text{CF}_3\text{Cl}$  could reduce  $\text{Cr}_2\text{O}_3$ , as hypothesized for our activation process. In an attempt to shed more light on this particular activation process we examined the reaction of  $\text{CF}_3\text{Cl}$  with  $\text{Cr}_2\text{O}_3$  in the TAP reactor. Upon pulsing  $\text{CF}_3\text{Cl}$  over a sample of  $\text{Cr}_2\text{O}_3$  that had been heated to 698 K we observed the formation of large amounts of  $\text{CHF}_3$ , identified by its characteristic mass spectra, and smaller amounts of  $\text{CO}_2$  and  $\text{H}_2\text{O}$ . Since we already knew that  $\text{CHF}_3$  was an effective activator of  $\text{Cr}_2\text{O}_3$ , this finding was sufficient to explain the formation of an activated catalyst following this treatment. However, the source of hydrogen has remained unknown. Possibly, hydrogen from surface hydroxyl groups reacted with  $\text{CF}_3\text{Cl}$  with an accompanying oxidation of an associated Cr site. The newly-formed  $\text{CHF}_3$  could then reduce already-existing high-valent Cr centers to

form the active catalyst sites. To test this we next treated a sample of  $\text{Cr}_2\text{O}_3$  with a flow of oxygen at 698 K in an attempt to oxidatively remove any such surface hydroxyl groups and any other surface reducing agents. Following this, we pulsed  $\text{CF}_3\text{Cl}$  over the freshly-treated  $\text{Cr}_2\text{O}_3$  and found no evidence of gaseous reaction products. Separately, a parallel experiment was carried out in our microreactor whereby a sample of  $\text{Cr}_2\text{O}_3$  was treated with 20%  $\text{O}_2$  in  $\text{N}_2$  at 698 K/1 h prior to treatment with 20%  $\text{CF}_3\text{Cl}$  in  $\text{N}_2$  at 698 K/1 h. Testing of the resulting catalyst under our standard test conditions at 323 K revealed an activity that was only 6% of the activity obtained previously from a  $\text{CF}_3\text{Cl}$ -activated catalyst obtained *without* pretreatment with  $\text{O}_2$ . From these results we conclude that  $\text{CF}_3\text{Cl}$  alone does not appear to reduce  $\text{Cr}_2\text{O}_3$  under these conditions but requires the presence of unknown surface reducing agents, such as hydroxyl groups.

In microreactor studies both  $\text{Cr}_2\text{O}_3$  and  $\text{Cr}_2\text{O}_3(\text{C})$ , following activation by CO at 698 K, proved to be active catalysts for disproportionation of  $\text{CHF}_2\text{Cl}$  at temperatures as low as 296 K (see Table 5). Under such mild conditions the formation of metal halide surface sites might be questioned. To explore

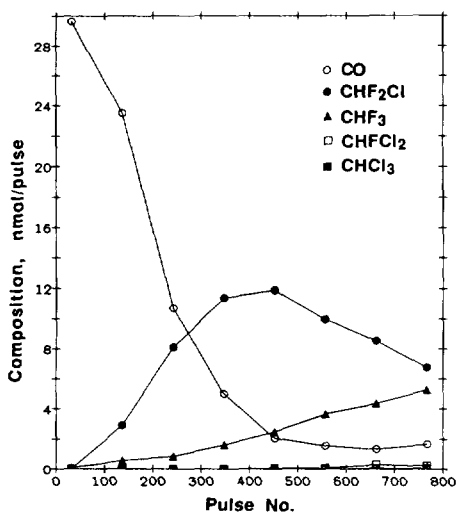


Fig. 5. Reaction of  $\text{CHF}_2\text{Cl}$  with CO-reduced  $\text{Cr}_2\text{O}_3$  as a function of pulse number.

this question we examined the reaction of  $\text{CHF}_2\text{Cl}$  with CO-reduced  $\text{Cr}_2\text{O}_3$  in the TAP reactor. We found that  $\text{CHF}_2\text{Cl}$ , when pulsed over CO-reduced  $\text{Cr}_2\text{O}_3$  at temperatures as low as 348 K, reacted to form CO. When  $\text{CHF}_2\text{Cl}$  was pulsed over CO-reduced  $\text{Cr}_2\text{O}_3$  at 523 K, CO ( $m/e = 28$ ) was the *only* product observed, initially. On further pulsing new unidentified products began to appear. These compounds yielded  $m/e$  values of 69, 51, and 47 and were tentatively identified as the fragments  $\text{CF}_2\text{OH}$ ,  $\text{CF}_2\text{H}$ , and  $\text{COF}$ . In order to verify that the CO was coming from  $\text{CHF}_2\text{Cl}$  and not from CO that had remained on the surface following the reduction step, we separately reduced  $\text{Cr}_2\text{O}_3$  with  $^{13}\text{CO}$  and showed that, upon pulsing  $\text{CHF}_2\text{Cl}$  over the reduced material, no evidence of enrichment of the natural abundance of the  $^{13}\text{C}$  in CO was found. After additional pulsing of these systems, disproportionation products began to appear while the formation of CO declined. Mass spectral analysis of the products arising from a sample of CO-reduced  $\text{Cr}_2\text{O}_3$ , following every 100 pulses, yielded the product composition evolution given in Fig. 5.

As seen from Fig. 5, the decline in the

formation of CO appears to be matched by a corresponding rise in disproportionation activity as evidenced by the rising formation of disproportionation products and a decline in the  $\text{CHF}_2\text{Cl}$  reactant, following an initial rise in  $\text{CHF}_2\text{Cl}$  due to its decreasing reaction with the surface. This is direct evidence that the active sites of the catalyst are created by the reaction of  $\text{CHF}_2\text{Cl}$  with the reduced chromium oxide surface. Measurements of the carbon balance associated with the reaction showed that approximately half of the carbon fed to the catalyst remained bound to the surface following a pulse. This probably occurred because the disproportionation products were strongly absorbed on the surface. This explanation was supported when the individual products, upon pulsing over unactivated  $\text{Cr}_2\text{O}_3$ , yielded increasing pulse intensities as the temperature was raised above 523 K. Evidence that the chromium sites reacting were those that were previously reduced by CO, at a higher temperature, was found when it was noted that unreduced  $\text{Cr}_2\text{O}_3$  did not significantly react with  $\text{CHF}_2\text{Cl}$  at 523 K to produce either CO or disproportionation products. Non-reduced  $\text{Cr}_2\text{O}_3$  produced less than 4% of the CO produced by the reduced  $\text{Cr}_2\text{O}_3$  at 523 K. Apparently, the CO that was produced by the nonreduced  $\text{Cr}_2\text{O}_3$  at 523 K was coming from nascent reduced sites created by the reduction of  $\text{Cr}_2\text{O}_3$  by  $\text{CHF}_2\text{Cl}$ , since low levels of  $\text{CO}_2$  production were also observed at this temperature.

(b) *Catalytic activity.* In a search for a direct link between  $\text{CO}_2$  formation and catalytic activity, we monitored the formation of  $\text{CO}_2$ ,  $\text{CHFCl}_2$ ,  $\text{CHF}_3$ , and  $\text{CHCl}_3$  in the TAP reactor at 798 K during activation of  $\text{Cr}_2\text{O}_3$  by  $\text{CHFCl}_2$ . The disproportionation of  $\text{CHFCl}_2$  was examined since it was easier to follow the formation of these products by mass spectroscopy than those from  $\text{CHF}_2\text{Cl}$  disproportionation. Data were acquired by sequentially measuring the mass spectral intensity of each component formed following the pulsing of  $\text{CHFCl}_2$  over the chrome oxide. Figure 6 presents the mass spectral

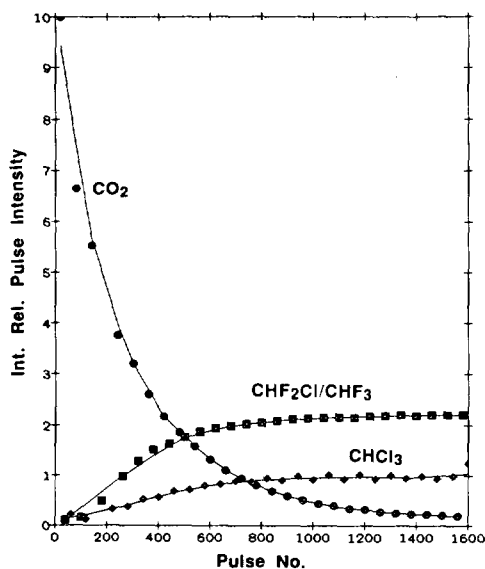


FIG. 6. Mass spectral areas vs pulse number for the reaction of  $\text{CHF}_2\text{Cl}$  with  $\text{Cr}_2\text{O}_3$ .

pulse areas for the three components:  $\text{CO}_2$ ,  $\text{CHCl}_3$ , and  $\text{CHF}_2\text{Cl}/\text{CHF}_3$ . This figure clearly shows that as the formation of carbon dioxide decreases, the activity of the catalyst towards disproportionation increases. This experiment supports our presumption that the creation of active sites in disproportionation catalysis involves a reduction of high-valent chromium ions.

An experiment was carried out in which we sought to examine the disproportionation of  $\text{CHF}_2\text{Cl}$  at its earliest stages over a chrome oxide sample that had been activated by treatment with  $\text{CHF}_3$ . Catalyst activation was accomplished by treating 70 mg of  $\text{Cr}_2\text{O}_3(\text{C})$  with a stream of 1 cc/min of  $\text{CHF}_3$  at 682 K for 1 h. By this treatment, if surface metal halides were formed, only metal fluorides would have been possible. Pulsing  $\text{CHF}_2\text{Cl}$  (ca. 5.3 nmole/pulse) over this activated material at 561 K showed that initially mostly  $\text{CHF}_3$  was formed. As the pulsing continued, increasing amounts of  $\text{CHFCl}_2$  and  $\text{CHCl}_3$  formed while the relative amounts of  $\text{CHF}_3$  formed decreased. Figure 7 shows the pulse compositions as

a function of number of pulses of  $\text{CHF}_2\text{Cl}$  introduced. While the F:Cl ratio was high (11.4) after 880 pulses, after 4000 pulses of  $\text{CHF}_2\text{Cl}$  the F:Cl ratio reached 2.30, close to the theoretical level of 2.0 required for the disproportionation. These results show that the disproportionation products can arise from independent reactions and are not formed in constant proportions as required by a bimolecular mechanism. We conclude that  $\text{CHF}_3$ -activated  $\text{Cr}_2\text{O}_3(\text{C})$  initially contains sites capable only of fluorination of a reactive HCFC. One may assume that sites active towards chlorination are then gradually introduced as surface halogen exchange proceeds during the reaction with a HCFC.

(c) *Lewis acidity.* In our microreactor studies we showed that the disproportionation of  $\text{CHF}_2\text{Cl}$  was inhibited by dimethyl ether, presumably acting as a Lewis base blocking Lewis acid sites responsible for the catalysis. As a follow-up to this discovery, we compared the Lewis acidities of untreated  $\text{Cr}_2\text{O}_3$  with those that had been reduced by  $\text{CHF}_3$  or CO through a temperature-programmed desorption measurement of dimethyl ether carried out in the TAP

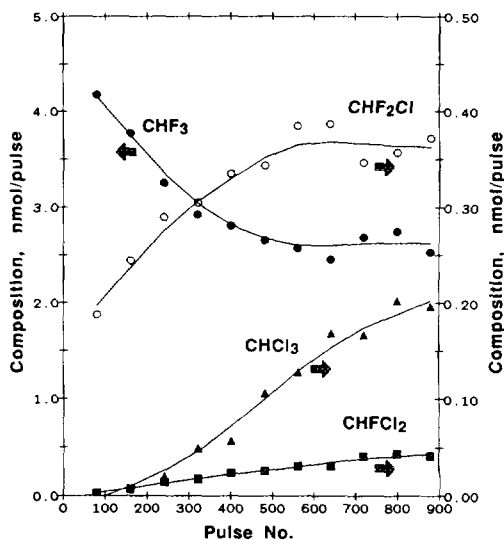


FIG. 7. Pulse composition as a function of number of  $\text{CHF}_2\text{Cl}$  pulses over  $\text{CHF}_3$ -treated  $\text{Cr}_2\text{O}_3(\text{C})$ .

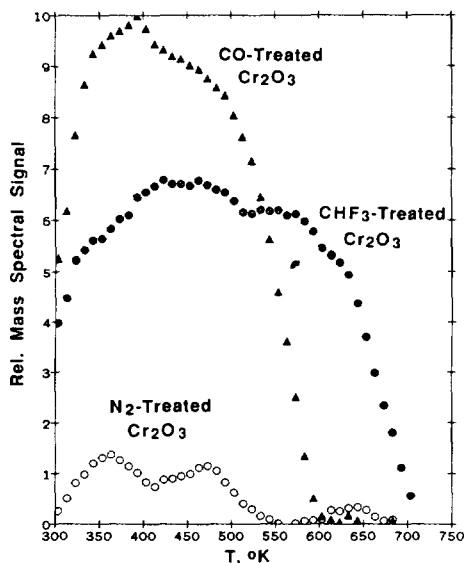


Fig. 8. Temperature-programmed desorptions of dimethyl ether from  $\text{Cr}_2\text{O}_3$ .

reactor. All of the samples were preheated to 798 K, treated with the appropriate treatment gas (none in the case of the untreated sample) and subsequently saturated with dimethyl ether at room temperature at  $10^{-5}$  Torr. Following this, each sample was heated at  $10^\circ/\text{min}$  while monitoring the relative amounts of dimethyl ether desorbing by measuring  $m/e = 46$  every second. Figure 8 shows the results obtained. As can be seen from this figure, treatment with either CO or  $\text{CHF}_3$  greatly increases the population of Lewis acid sites. This is further support for the hypothesis that Lewis acid sites are necessary for catalysis to occur. Also, the extensive desorption at high temperatures shown by the  $\text{CHF}_3$ -treated sample suggests the presence of relatively strong Lewis acid sites, probably resulting from site fluorination.

Further support for the increase in Lewis acidity on reduction came from an examination of the peak shapes of  $\text{CO}_2$  resulting from the reduction of  $\text{Cr}_2\text{O}_3$  with CO. On pulsing untreated  $\text{Cr}_2\text{O}_3$  with CO, very sharp  $\text{CO}_2$ -product pulses were detected initially that

became broader as the extent of reduction (i.e., number of CO pulses injected) increased. The absolute width of the product  $\text{CO}_2$ -pulse increased by fivefold over the course of the reduction. This increase in peak width can best be attributed to the increasing strength of adsorption at reduced sites on the catalyst surface.

(d) *Kinetic order.* A bimolecular disproportionation mechanism should exhibit a second order dependence on  $\text{CHF}_2\text{Cl}$ , at least at low surface coverages, if the halogen exchange reaction is the rate-determining step. As a test of this hypothesis, we examined the dependence of the rate of formation of  $\text{CHF}_2\text{Cl}$  reaction products on the integrated pulse intensity of the  $\text{CHF}_2\text{Cl}$  fed to the reactor over  $\text{Cr}_2\text{O}_3$  which had been activated and equilibrated by treatment with  $\text{CHF}_2\text{Cl}$  at 698 K. As a measure of the reaction rate, the initial amount of  $\text{CHF}_3$  formed (proportional to its rate of formation) vs. integrated  $\text{CHF}_2\text{Cl}$  pulse intensity was examined. A full composition measurement was carried out at each pulse intensity to insure an accurate measure of the  $\text{CHF}_3$  composition. After applying a small linear correction to account for variations in average residence time in the reactor (resulting from a transition from Knudsen diffusion to viscous flow), the data was fitted to a simple non-integral power model. We found the order for the reaction (*c.f.* Appendix) to be  $0.91 \pm 0.06$  indicating the absence of a bimolecular mechanism, if halogen exchange is the rate-determining step in this process. Figure 9 summarizes our findings.

#### DISCUSSION

The chrome oxides used in this study as catalysts for the disproportionation of  $\text{CHF}_2\text{Cl}$  apparently are required to undergo at least two separate surface transformations before becoming catalytically active. The first transformation involves a surface reduction as indicated by the oxidation of such reducing agents as CO and  $\text{H}_2$  at elevated temperatures. This reaction of nominally  $\text{Cr}^{3+}$  oxides is not a new reaction hav-

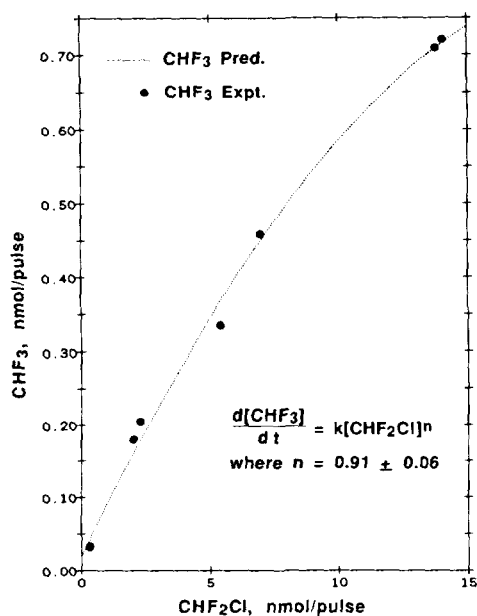


FIG. 9. CHF<sub>2</sub>Cl reacting at various pulse intensities over Cr<sub>2</sub>O<sub>3</sub> to yield CHF<sub>3</sub>.

ing been observed by other workers investigating other catalytic reactions of these oxides (14, 20, 25) and related chromia/aluminas (27, 28). For example, Winfield *et al.* (14), have observed the reaction of chromia catalysts with hydrogen and ascribed this reaction to reduction of Cr<sup>4+</sup> and Cr<sup>6+</sup> surface sites. The oxidants are generally agreed to be high-valent Cr sites present on the surface of chromia-based catalysts. The resulting reduced sites are expected to be powerful Lewis acid sites since they should possess high positive charge densities resulting from the stripping of oxygen from the metal atoms by the reductants. This is borne out by the observed increase in Lewis acidity of these oxides upon reduction by CO, as measured by dimethyl ether temperature-programmed desorption. The second transformation appears to involve the reaction of these highly reactive reduced sites with an HCFC to yield halogenated metal sites. In addition, the surface Lewis acidity appears to undergo a further increase, as noted above, when CHF<sub>3</sub> was used as an activator.

The formation of the metal halide sites is implied by the formation of CO as the major reaction product during the initial stages of the reaction of CHF<sub>2</sub>Cl with CO-reduced Cr<sub>2</sub>O<sub>3</sub>. Using <sup>13</sup>CO, the CO produced was also shown to not result from CO that might have been left behind from the CO reduction step. However, the absence of HF or HCl among the volatile products of the second transformation indicates that at least some of the halogen is present on the surface as complexed HF or HCl. The fact that hydrogen halides were observed as volatile products at higher temperatures suggests that these products were not irreversibly bound to the surface. Finally, our XPS results clearly indicate the presence of chromium fluorides on the surface of CHF<sub>3</sub>-treated Cr<sub>2</sub>O<sub>3</sub>.

The valence states of the active chromium sites both prior to and following these transformations are not well defined. However, the formation of both Cr<sup>2+</sup> and Cr<sup>3+</sup> following the reduction of high-valent chrome oxide sites by CO is well documented for both α-Cr<sub>2</sub>O<sub>3</sub> and α-Cr<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> mixtures (20, 27, 28). Importantly, coordinatively unsaturated Cr<sup>2+</sup> sites formed on Cr<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> surfaces in this manner have been reported to be rapidly oxidized by O<sub>2</sub> or H<sub>2</sub>O at ambient temperatures (27, 28). As noted above, the disproportionation reaction is not affected by the addition of oxygen, either prior to or during the feeding of CHF<sub>2</sub>Cl to the catalyst at 323 K. Also, treatment of CO-reduced Cr<sub>2</sub>O<sub>3</sub> with water at 698 K yielded a catalyst possessing *ca.* half the activity of an untreated control sample. The reduction in activity noted could have been the result of partial site blockage by adsorbed water. If Cr<sup>2+</sup> sites are necessary for catalysis to occur, then no activity should have been observed in either case. Finally, CO, but no reduction products, such as H<sub>2</sub>, H<sub>2</sub>CO, or CHF<sub>2</sub>CHF<sub>2</sub>, were observed on reaction of CHF<sub>2</sub>Cl with CO-reduced Cr<sub>2</sub>O<sub>3</sub>, indicating the CHF<sub>2</sub>Cl is not reduced by the chromium surface. The well-known reducing properties of Cr<sup>2+</sup> salts towards alkyl halides (29)

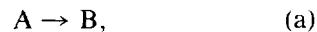
would suggest that a rapid reduction of  $\text{CHF}_2\text{Cl}$  should occur under our reaction conditions if significant quantities of  $\text{Cr}^{2+}$  sites were present. No such reactions were observed. Thus, this lack of evidence for reduction products suggests that the valence state of chromium following the first transformation is probably largely  $\text{Cr}^{+3}$  and remains unchanged during the second transformation. Importantly, while  $\text{Cr}^{+2}$  may be present following the first transformation, it does not appear to be required for catalysis to occur. The initial valence state(s) of the chromium sites that are reduced during the first transformation is also uncertain. However, as noted above, the precursors to the active sites are *non-water-soluble* higher-valent Cr species. This could mean that these precursor sites are  $\text{Cr}^{4+}$  or  $\text{Cr}^{5+}$  sites and not  $\text{Cr}^{6+}$  sites, although non-soluble  $\text{Cr}^{6+}$  species are possible.

Our results lead us to propose coordinatively-unsaturated  $\text{Cr}^{3+}$  centers as necessary components of the active sites of the disproportionation reaction of  $\text{CHF}_2\text{Cl}$  over chrome oxides. In addition, we feel that these centers must contain Cr-X (X = F or Cl) bonds, leading to an enhancement of the Lewis acidity of these centers. While a detailed description of a mechanism is not possible from our data, the kinetic evidence does rule out a Rideal-Eley mechanism where a free organic species reacts with a surface-bound organic species in the rate-determining step. Unfortunately, a kinetic model corresponding to a monomolecular halogen-exchange reaction of HCFCs with metal halide sites, as given by our halogenated-site model, could not be tested due to the complexity of the model. However, evidence that the disproportionation of  $\text{CHF}_2\text{Cl}$  does not follow a bimolecular mechanism, where two  $\text{CHF}_2\text{Cl}$  molecules simultaneously exchange their halogens, comes from the TAP study showing the formation of varying ratios of the disproportionation products in the initial phases of the disproportionation. Finally, in preliminary studies, we have shown that the treatment of

$\text{Cr}_2\text{O}_3$  with reducing agents acts to produce a catalyst active in the fluorination of  $\text{CHF}_2\text{Cl}$  with HF. Thus, the chromia sites responsible for HCFC disproportionation are very likely the same ones responsible for fluorination reactions of these materials.

#### APPENDIX

The determination of the kinetic orders of a reaction occurring during the passage of a pulse of reactant through a packed catalyst bed, as in the TAP reactor, may be carried out using a variety of explicit physical models (30). However, these models are sometimes difficult to apply in practice and approximate methods are often useful. An approximate model, applicable to the TAP reactor experiments described above, is described here which allows one to determine the order of a reaction in a reactant or product using a minimal set of data. This model shall be derived for the simple reaction,



where A is a gaseous reactant and B a gaseous product. It is further assumed that the microscopic rate law for this reaction may be given by a power-law rate expression of the form

$$\text{Rate of formation of B} = k_r A(A_0, S_0, T, x, t, k)^n, \quad (\text{b})$$

where  $A(A_0, S_0, T, x, t, k)$  represents the concentration of A along the reactor bed and where  $A_0$  represents the initial concentration of A at the entrance to the bed and  $S_0$ , the surface concentration of active catalyst sites. The reaction rate constant is given by  $k_r$ . Temperature,  $T$ , time,  $t$ , axial position along the reactor,  $x$ , and various system rate constants,  $k$ , represents additional parameters (in an effort to minimize this cumbersome notation, only a limited variable set will be included in the formulas below). This model assumes that all parameters are independent of the radial coordinates.

A frequently-measured quantity in a typical TAP experiment is the quantity  $Q_B$ , the



total amount of the material B formed following the passage of a pulse of A through the reactor.  $Q_B$  may be described by the expression

$$\begin{aligned} Q_B &= Q_{B_0} + \sigma \int_0^{t_p} \int_0^L (\text{Rate of reaction}) dx dt \\ &= Q_{B_0} + \sigma \int_0^{t_p} \int_0^L k_r A(A_0, T, x, t)^n dx dt, \end{aligned} \quad (c)$$

where the reaction rate is integrated over the length,  $L$ , of the reactor and the time period,  $t_p$ , over which the measurements are taken. This time period is arbitrary but may be taken to be a time over which >99% of the reactant A has passed through the reactor. The quantity  $\sigma$  is the cross-sectional area of the reactor. The quantity  $Q_{B_0}$  is the initial quantity of B fed to the reactor.

Using Eq. (c) we may define expressions from which the kinetic order,  $n$ , of this process may be determined. In order to accomplish this, we need first to establish conditions under which the dependence of  $A(A_0, T, x, t)$  on  $A_0$  may be defined. While the form of the function  $A(A_0, T, x, t)$  is unknown, we may expand this function as a power series in  $A_0$  in order to quantify its dependence on  $A_0$ :

$$A(A_0, T, x, t) = \sum_{i=1}^{\infty} \alpha_i(T, x, t) A_0^i \quad (d)$$

As a first-order approximation, we may express A as the first term in the above series,

$$A(A_0, T, x, t) = \alpha_1(T, x, t) A_0, \quad \text{where } 0 \leq \alpha_1(T, x, t) \leq 1. \quad (e)$$

For an unreacting gas, at constant temperature, this approximation is equivalent to assuming that the average residence time of a gas passing through the reactor is independent of the amount of gas present. This turns out to be a good approximation when the partial pressure of the gas is low enough to be in the Knudsen flow regime since in this regime both experiment and theory show a virtual lack of dependence of average resi-

dence time on the quantity of gas present in a pulse (21). Even for partial pressures somewhat higher than this the approximation remains good, in our experience. However, when a gas is reacting, the dependence on  $A_0$  must also include the effects of reaction. Obviously, when changes in  $A(A_0, T, x, t)$  are small, due to low conversions of A to products, then eq. e should remain a good approximation. A special case, however, occurs when A reacts by a first-order process. In this case, any linear dependence of  $A(A_0, T, x, t)$  on  $A_0$  due to reaction is reinforced by the inherent linearity of A on  $A_0$  in first-order processes. Thus, even at relatively high conversions of A, Eq. (e) probably remains a good approximation to A in this case.

Using the approximation given by Eq. (e), Eq. (c) becomes

$$Q_B = Q_{B_0} + \sigma A_0^n \int_0^{t_p} \int_0^L k_r \alpha_1(T, x, t)^n dx dt. \quad (f)$$

At low conversions of A to products, the integral in Eq. (f) remains relatively constant (at constant temperature) as  $A_0$  is varied, with  $\alpha_1(T, x, t)^n$  varying between zero and unity,

$$\begin{aligned} Q_B &= Q_{B_0} + \sigma A_0^n \int_0^{t_p} \int_0^L k_r \alpha_1(T, x, t)^n dx dt \\ &= Q_{B_0} - \sigma A_0^n F_1 \end{aligned} \quad (g)$$

$$\begin{aligned} n &= \frac{\ln(Q_{B_0} - Q_B) - \ln \sigma F_1}{\ln A_0} \\ &= \frac{\ln(Q_{B_0} - Q_B) - K}{\ln A_0}, \end{aligned} \quad (h)$$

where  $F_1$  is the integral factor and  $K$  is a parameter determined by the experimental data. Thus, by simply varying  $A_0$  and measuring  $Q_B$ , the order,  $n$ , of the reaction in A may be easily determined.

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